

Predictive Model for Nonlinear Resilient Modulus of Emulsified Asphalt Treated Base

Peng Li, Ph.D
Chang'an University

Jenny Liu, Ph.D, P.E.
University of Alaska Fairbanks

May 28, 2014



GeoShanghai 2014

Outline

- Background
- Experimental Design
- Test Results and Analysis
- Predictive Equation
- Conclusion

Background

- ATBs is the most commonly used stabilized layers because of available local asphalt resource
- Problem - lack of engineering characteristics for typical Alaskan ATBs
- Need - properly characterize these materials to better understand the effects of asphalt content on ATB behavior and provide accurate M_R values for flexible pavement design



Experimental Design

Source	Abrasion Resistance (% Loss)	Percent Fractured Face (one fractured face)		Flat or Elongated Pieces (5:1)	
		Test Results	Requirement	Test Results	Requirement
Southeast Region	9.7%	100%	≥80%	3%	≤8%
Central Region	5.8%	91.7%		0	
Northern Region	2.7%	84.5%		0	

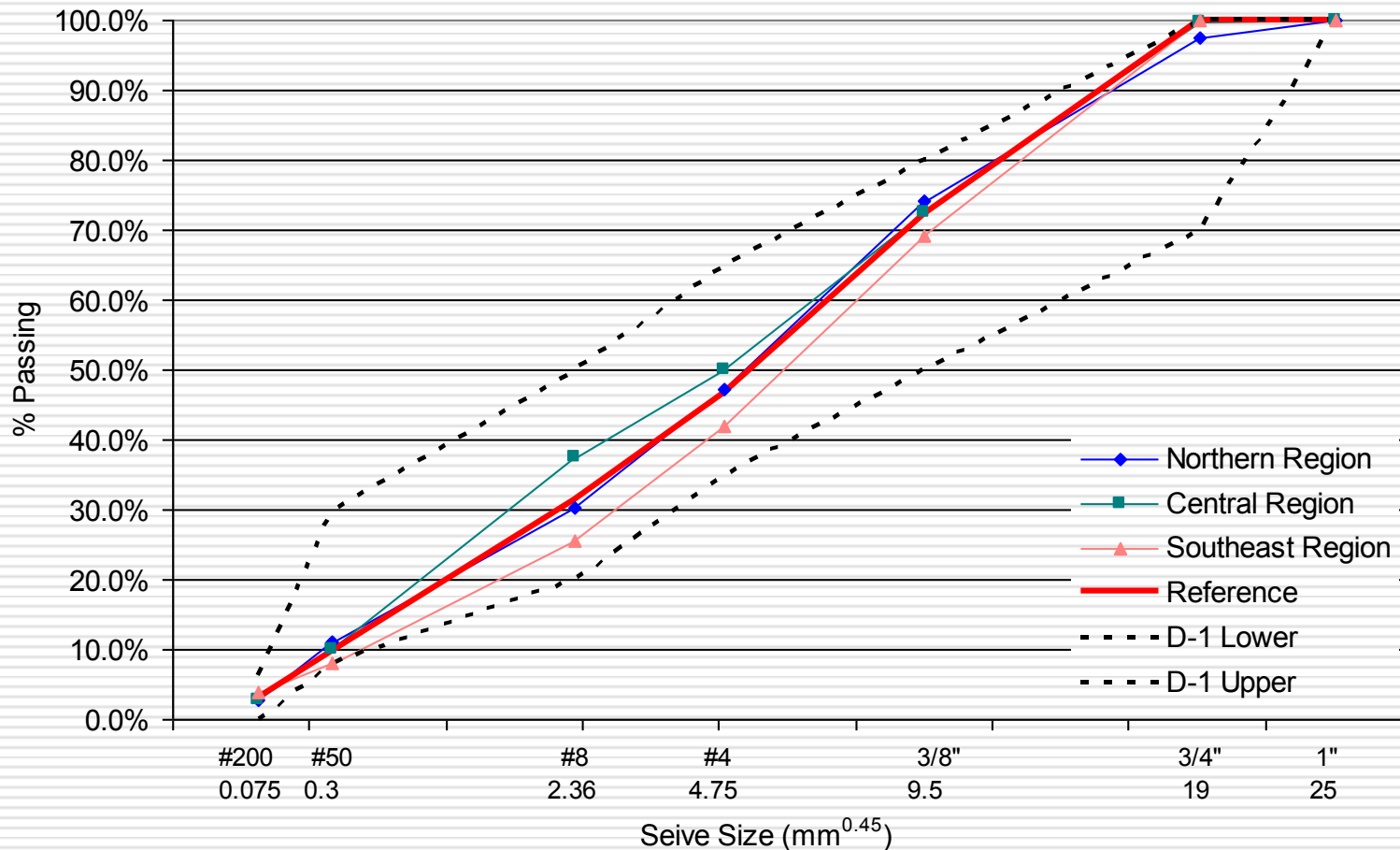


Northern

Central

Southeast

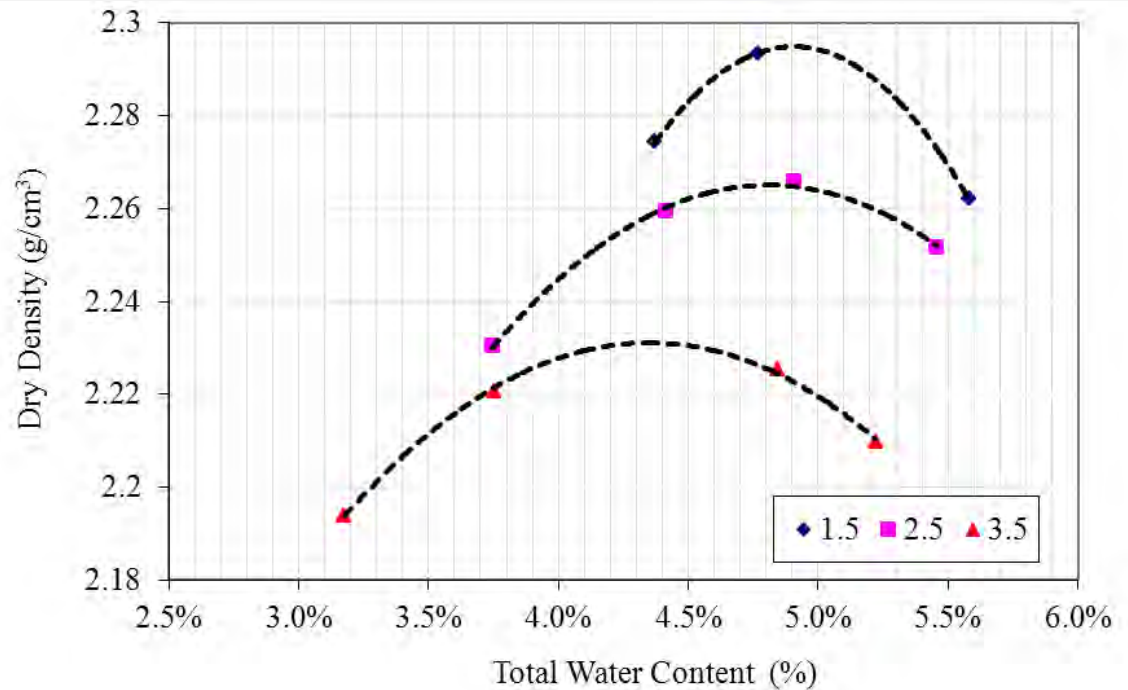
Experimental Design (Continued)



Experimental Design (Continued)

Compaction:

- ASTM D1557
- At "pseudo OMC"
- Diameter: 100mm
- Height: 150mm

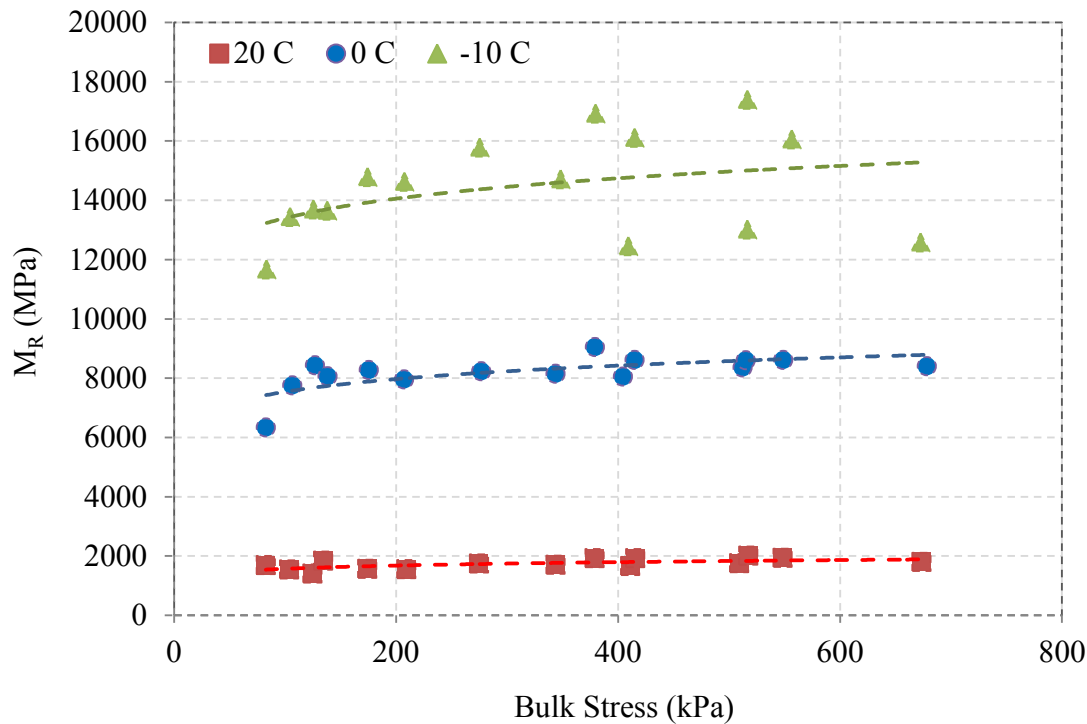


Experimental Design (Continued)



Testing Equipment Setup

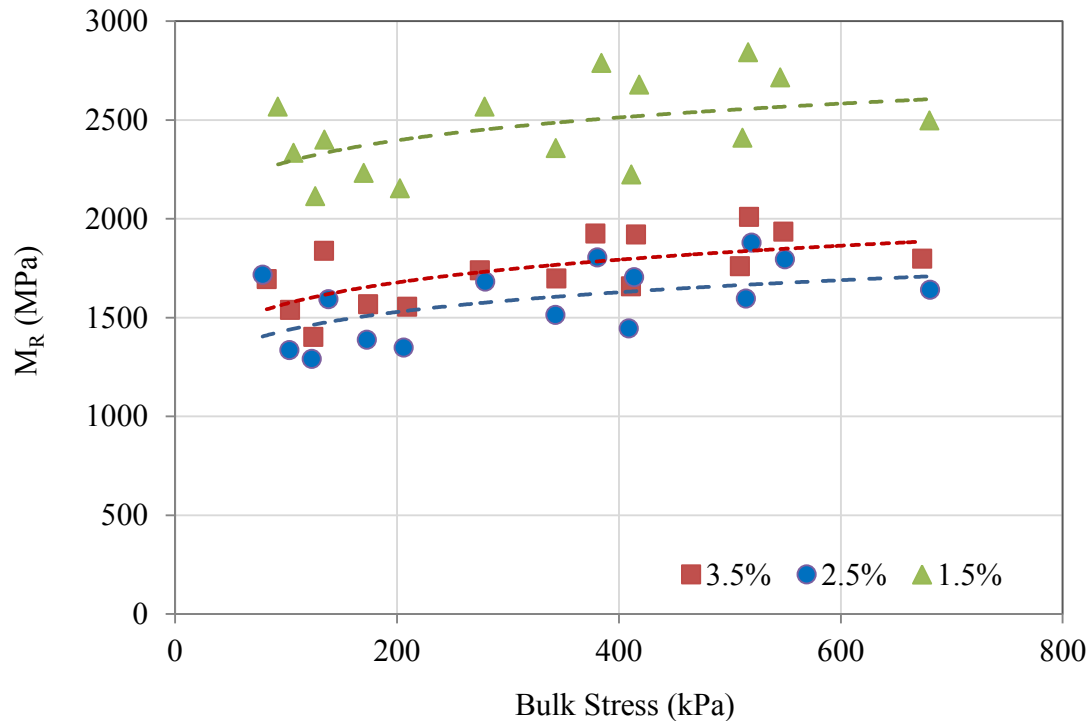
Test Results and Analysis



Effects of Temperature on MR of EATB
(Northern Region, 3.5% Residual Binder)

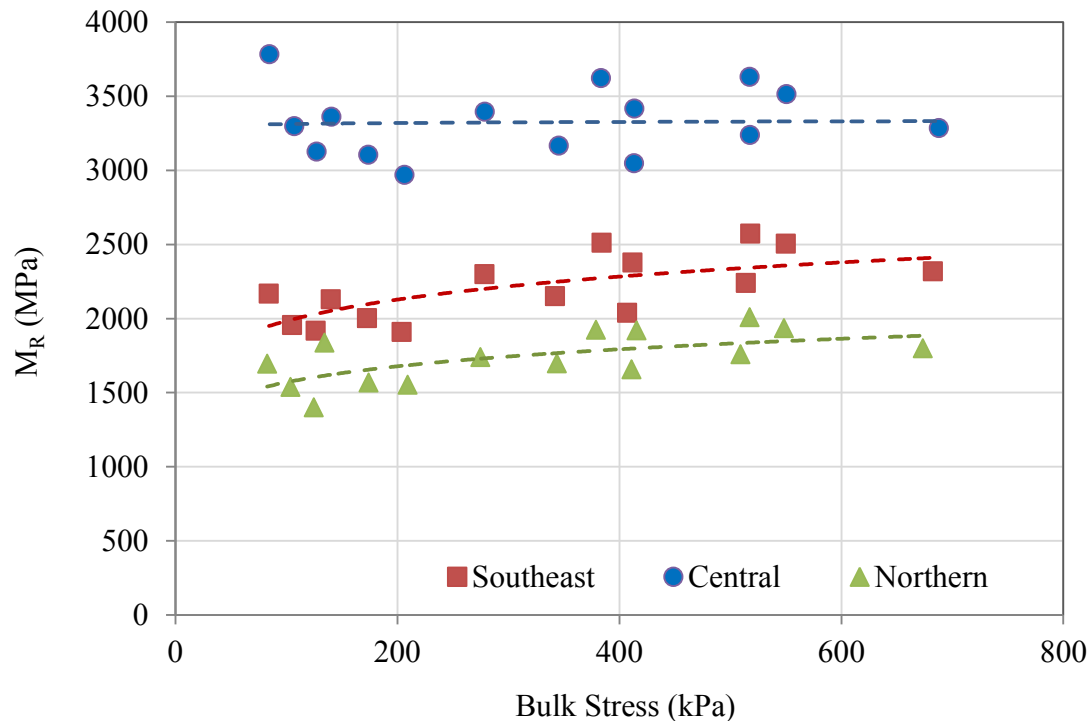
Test Results and Analysis

(Continued)



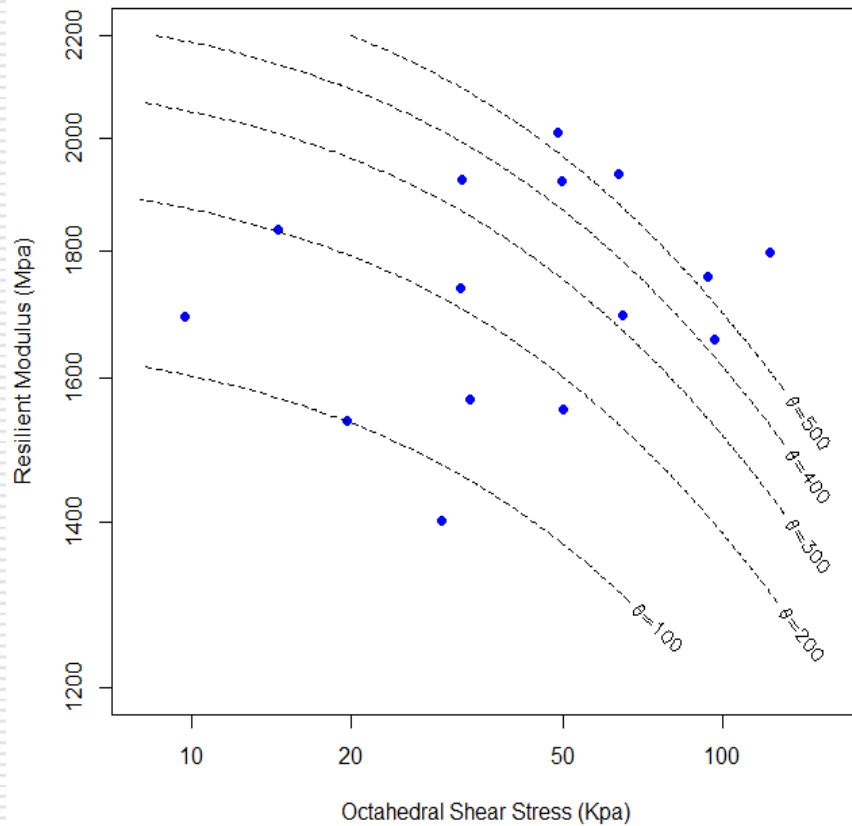
Effects of Binder Content on MR of EATB
(Northern Region, 20°C)

Test Results and Analysis (Continued)

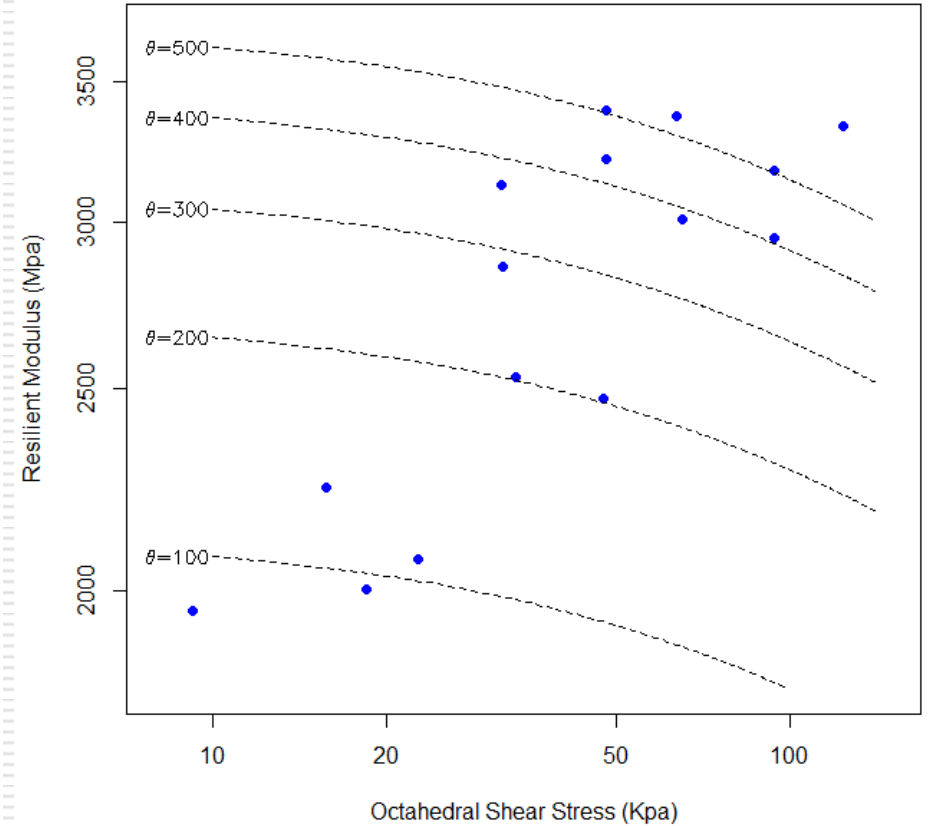


Effects of Aggregate Source on M_R of EATB
(20°C, 3.5% Residual Binder)

Stress Dependent Property (20°C, 3.5% Binder, Northern Region)

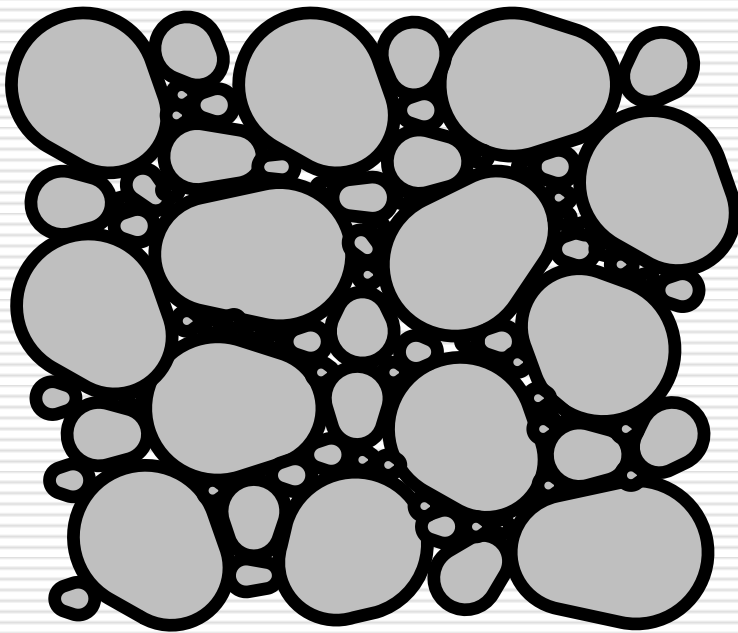


EATB

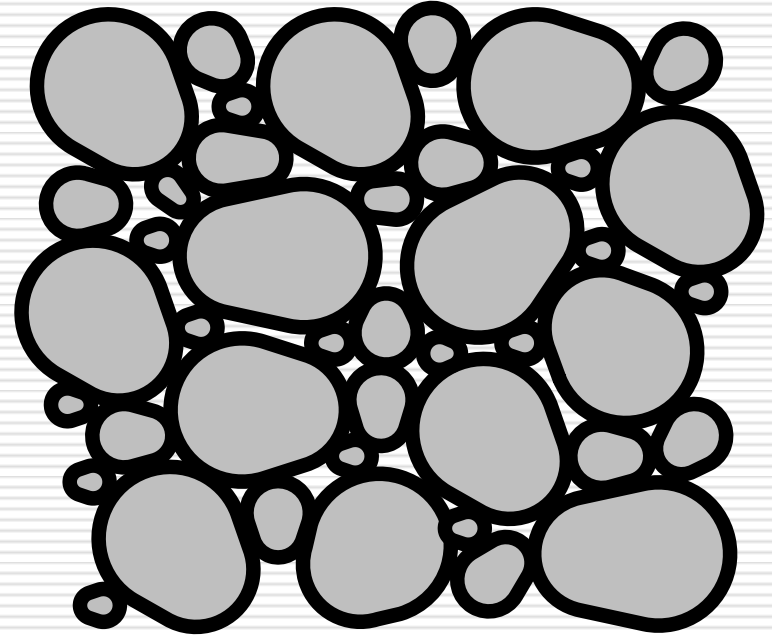


HATB

Internal Structure Sketches of HATB and EATB

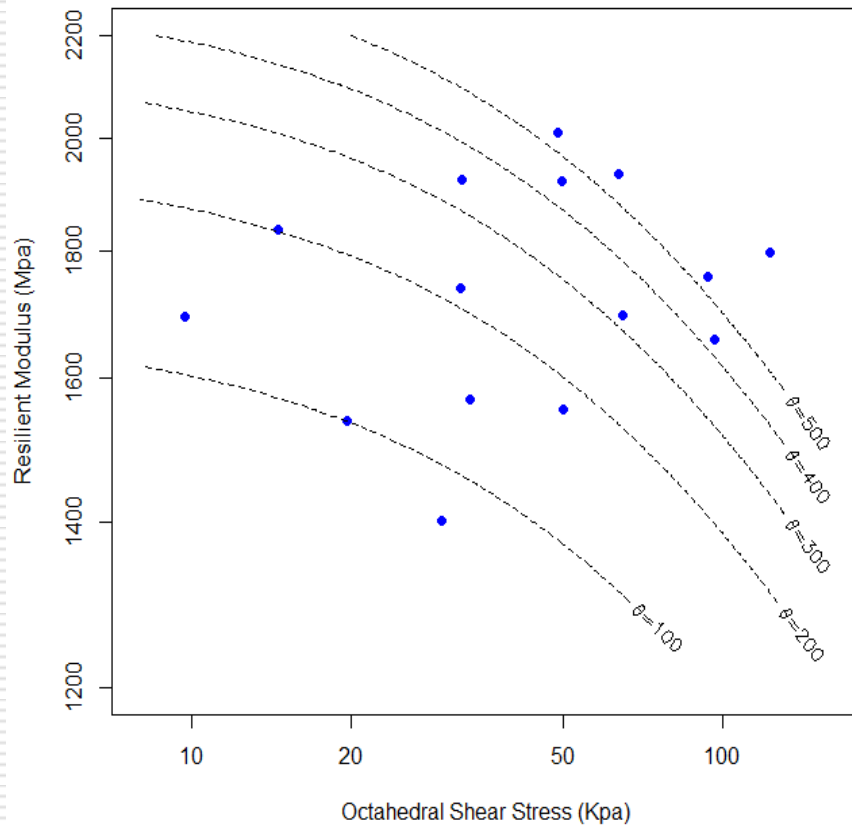


HATB

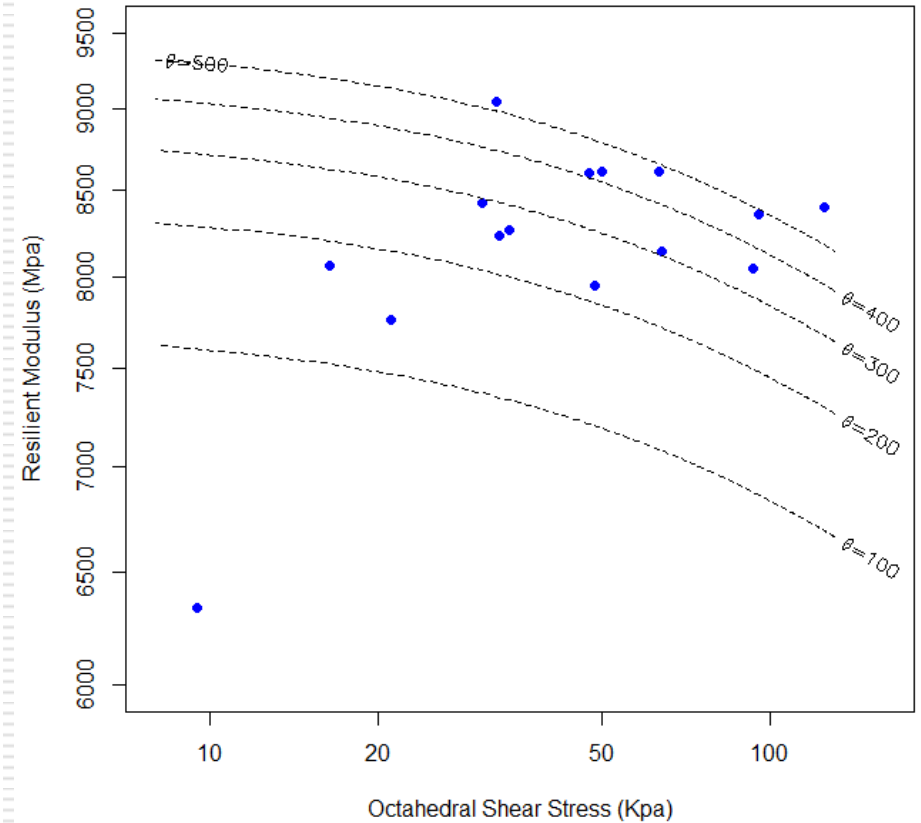


EATB

Stress Dependent Property (3.5% Binder, Northern Region)



EATB, 20°C,

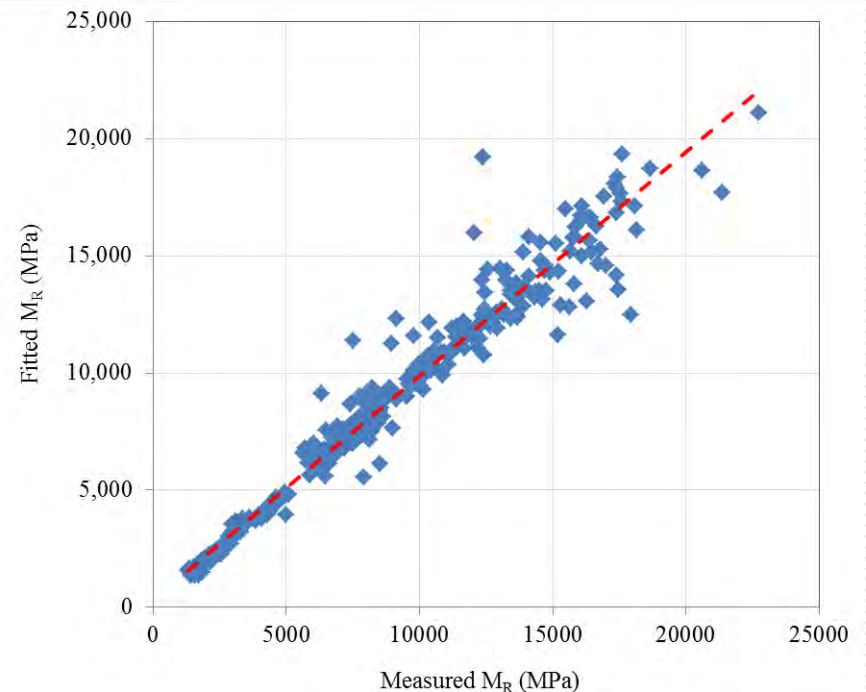
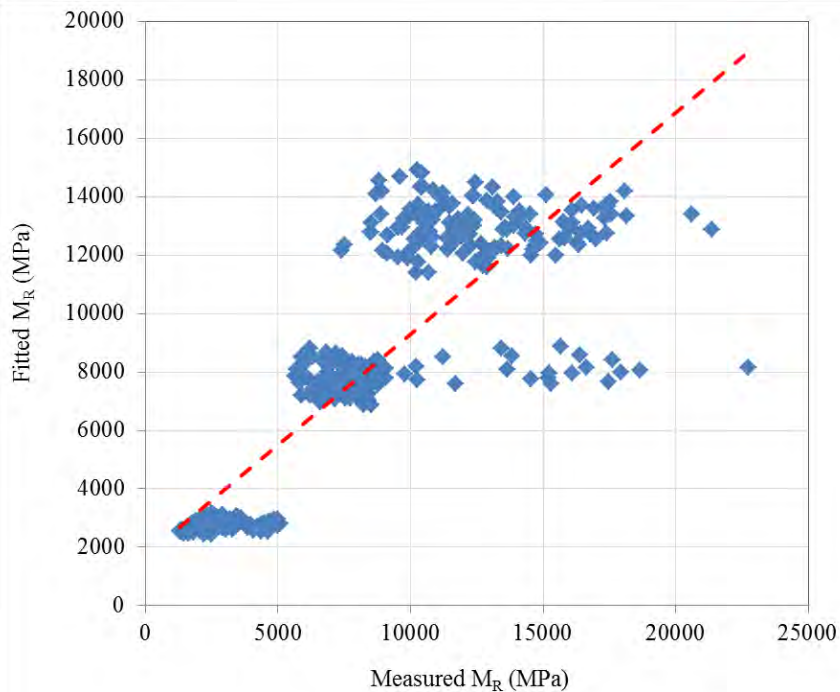


EATB, 0°C

Predictive Equation



$$M_R = k_1 P_a \left(\frac{\theta}{P_a} \right)^{k_2} \left(\frac{\tau_{oct}}{P_a} + 1 \right)^{k_3} \quad \text{MEPDG}$$

$$\ln(M_R) = a_0 + a_1 F + a_2 T + a_3 P_b + (b_0 + b_1 F + b_2 T + b_3 P_b) \ln\left(\frac{\theta}{P_a}\right) + (c_0 + c_1 F + c_2 T + c_3 P_b) \ln\left(\frac{\tau_{oct}}{P_a} + 1\right)$$



Conclusions

- M_R increases as:

Bulk Stress  Shear Stress 

Temperature  Aggregate Angularity 

- Predictive Model was proposed.

